

SANYO Semiconductors DATA SHEET

An ON Semiconductor Company

LV5029MD — LED Driver IC for LED Lighting

Overview

LV5029MD is a High voltage LED drive controller which drives LED current with external MOSFET. LV5029MD is realized very simple LED circuits with a few external parts. It corresponds to active power factor corrector control.

Note) This LV5029MD is designed or developed for general use or consumer appliance. Therefore, it is NOT permitted to use for automotive, communication, office equipment, and industrial equipment.

Functions

- High voltage LED controller
- Various Dimming Control -Analog Input & PWM Input
- Selectable Switching frequency
- [50 kHz or 70 kHz, open: 50 kHz]
- Built-in overvoltage detection of CS pin.
- Built-in active power factor corrector.

- Short protection circuit
- Selectable reference Voltage -Internal 0.605V & External Input Voltage
- Low noise switching system/skip frequency function
- 5 stages skip mode Frequency
- Soft driving

Specifications

Maximum Ratings at $Ta = 25^{\circ}C$

Parameter	Symbol	Conditions	Ratings	Unit
Maximum input voltage	V _{IN} max (Note1)		-0.3 to 42	V
REF_OUT, REF_IN, RT, CS, PWM_D			-0.3 to 7	V
OUT pin	V _{OUT} _abs		-0.3 to 42	V
Allowable power dissipation	Pd max	With specified board*	1.0	W

Continued on next page.

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LV5029MD

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Parameter	Symbol	Conditions	Ratings	Unit
Junction temperature	Тј		150	°C
Operating junction temperature	Topj (Note2)		-30 to +125	°C
Storage temperature	Tstg		-40 to +150	°C

*1 Specified board: 58.0mm × 54.0mm × 1.6mm (glass epoxy board)

Note1) Absolute maximum ratings represent the values which cannot be exceeded for any length of time.

Note2) Even when the device is used within the range of absolute maximum ratings, as a result of continuous usage under high temperature, high current, high voltage, or drastic temperature change, the reliability of the IC may be degraded. Please contact us for the further details.

Recommended Operating Conditions at $Ta = 25^{\circ}C$

Parameter	Symbol	Conditions	Ratings	Unit
Input voltage	VIN		8.5 to 24	V

* Note : supply the stabilized voltage.

Electrical Characteristics at Ta = 25°C, V_{IN} = 12V, unless otherwise specified.

Parameter	Symbol	Conditions		Ratings		Unit
Parameter	Symbol	Conditions	min	typ	max	Unit
Reference voltage block						
Built-in reference voltage	VREF		0.585	0.605	0.625	V
VREF VIN line regulation	VREF_LN	V _{IN} = 8.5 to 24V		±0.5		%
Reference output voltage	REFOUT	IREFOUT = 0.5mA		3.0		V
- Maximum load	REFOUT_MAX		0.5			mA
- equivalent output impedance	REFOUT_RO			10		Ω
Under voltage lockout		•				
Operation start Input voltage	UVLOON		8	9	10	V
Operation stop input voltage	UVLOOFF		6.3	7.3	8.3	V
Hysteresis voltage	UVLOH			1.7		V
Oscillation	•	•				
Frequency	FOSC1	RT =OPEN	40	50	60	kHz
	FOSC2	RT = REF_OUT	55	70	85	kHz
FOSC1 Switch voltage	V _{OSC} 1		2		5	V
FOSC2 Switch voltage	V _{OSC} ²				0.5	V
Maximum ON duty	MAXDuty			93		%
Comparator		•				
Input offset voltage	V _{IO_} VR			1	10	mV
(Between CS and VREF)						
Input offset voltage	V _{IO_} RI			1	10	mV
(Between CS and REFIN)	1			100		-
Input current				160		nA
00 sis manualtana	IIOREF			80	4	nA V
CS pin max voltage	VOM			150	1	
malfunction prevention mask time	TMSK			150		ns
PWM_D circuit						
OFF voltage	VOFF		2		5	V
ON voltage	VON		0		0.6	V
Thermal protection circuit	ÖN		_			
Thermal shutdown temperature	TSD	*Design guarantee		165		°C
Thermal shutdown hysteresis	ΔTSD	*Design guarantee		30		°C
Drive Circuit	-		1			
OUT sink current	lol		500	1000		mA
OUT source current	1 ₀ 0			120		mA
	TMIN			200	300	

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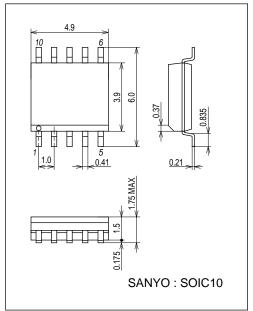
Deservator	Ourseland	Que ditions		Ratings			
Parameter	Symbol	Conditions	min	typ	max	Unit	
VIN current							
UVLO mode VIN current	I _{IN} OFF	V _{IN} < UVLOON		80	120	μA	
Normal mode V _{IN} current	I _{IN} ON	V_{IN} > UVLOON, OUT = OPEN		0.8		mA	
VIN over voltage protection ci	rcuit						
V _{IN} over voltage protection voltage	V _{IN} OVP		24	27	30	V	
VIN current at OVP	I _{IN} OVP	V _{IN} = 30V	0.7	1.0	1.5	mA	
CS terminal abnormal sensing	g circuit						
Abnormal sensing voltage	CSOCP			1.9		V	

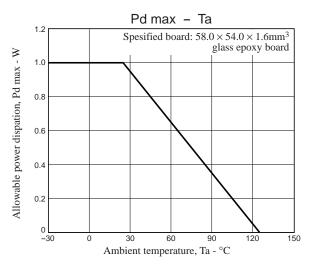
*: Design guarantee (value guaranteed by design and not tested before shipment)

Package Dimensions

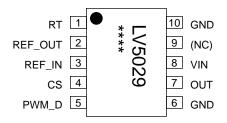
unit: mm (typ)

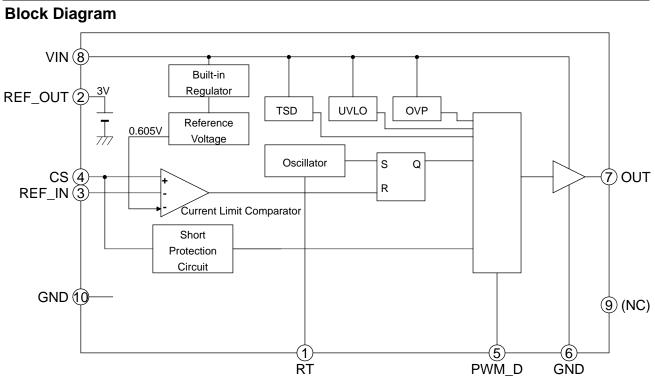
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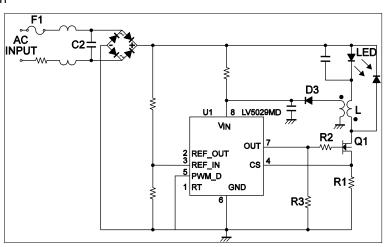
Pin Assignment



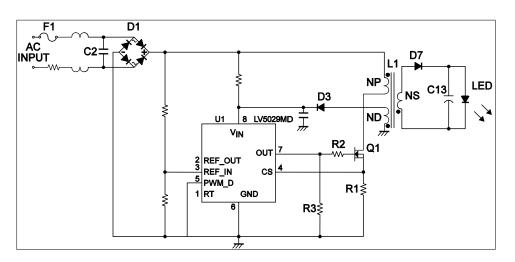


Sample Application Circuit

Non isolation



Isolation



Pin F	unctions		
Pin No.	Pin name	Pin function	Equivalent circuit
1	RT	Switching frequency selection pin. L or Open : 50kHz switching, H: 70 kHz switching. In case of 70kHz, connect to RT pin to REFOUT pin. on time	REF-OUT (3V typ) RTO GND O
2	REF_OUT	Built-in 3V Regulate out Pin. If this function isn't used, please connect to nothing.	O VIN C REF-OUT (3V typ) C GND
3	REF_IN	External LED current Limit Setting pin. If less than VREF (0.61V) voltage is input, Peak current value is used at the input voltage. If more than REF_IN voltage is input, it is done at VREF voltage. If this function isn't used, please connect nothing.	CSO-W-CSO-W-COREF_IN CSO-W-COREF_IN CSO-W-COREF_IN CSO-W-COREF_IN CSO-W-COREF_IN
4	CS	LED current sensing in. If this terminal voltage exceeds VREF (Or REF_IN), external FET is OFF. And if the voltage of the terminal exceeds 1.9V, LV5029MD turns to latch-off mod	
5	PWM_D	PWM Dimming pin. L or open: normal operation, H: Stop operation.	VIN PWM_D
6	GND	GND pin.	
7	OUT	Driving the external FET Gate Pin.	
8	VIN	Power supply pin. Operation : V _{IN} > UVLOON Stop: V _{IN} < UVLOOFF Switching Stop : V _{IN} > V _{IN} OVP	
9	NC	Connect to nothing	
10	GND	GND pin.	

LED current and inductance setting

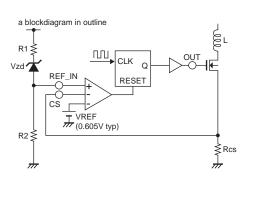
• Relation ship between REF_IN and CS pin voltage (Power Factor Correction (PFC))

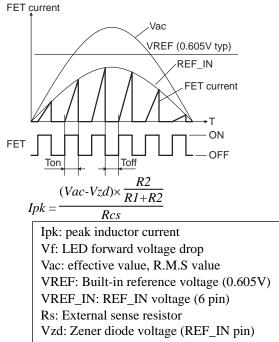
The output current value is the average of the current value that flows during one cycle. The current value that flows into coil is a triangular wave shown in the figure below. Make sure to set Ipk so that (average of current value at one cycle) is equal to (LED current value). Ipk is set by the relationship between REF_IN voltage and Rcs voltage. This relationship make Power Factor Correction (PFC). Therefore, it is available to make LED current a sine curve.

• Setting Zener voltage

Vzd depend on LED voltage (VF). Choose Zener diode around Vf (LED voltage).When VAC voltage is lower than Vf, LED operation is not normal. Using Zener diode prevents incorrect operating during VAC voltage lower than Vf. In detail, refer to [LED current and inductance setting]

In case of REF_IN pin open, this error amplifier negative input(-) is under control of internal VREF voltage (0.605Vtyp).



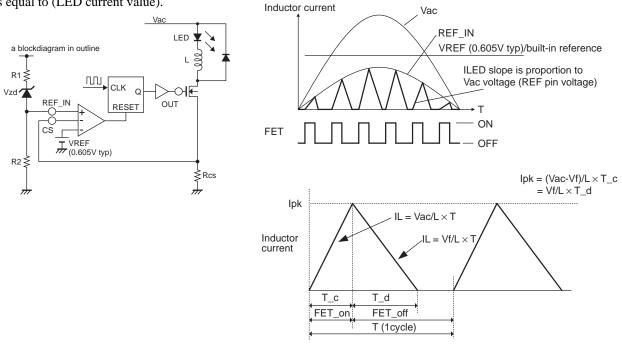


LED current and inductance setting

It is available to use both no-isolation and isolation applications.

(For non-isolation application)

The output current value is the average of the current value that flows during one cycle. The current value that flows into coil is a triangular wave shown in the figure below. Make sure to set IL_PK so that (average of current value at one cycle) is equal to (LED current value).



Given that the period when current flows into coil is T c + T d

 $DutyI = \frac{T_c+T_d}{T}$ $Ipk \times \frac{1}{2} \times (Duty \times T)/T = ILED$ $Ipk \times \frac{2 \times ILED}{DutyI} \quad (1) \text{ since } Ipk \times \frac{VREF_IN}{Rcs}$ $Rcs \times \frac{VFEF_IN}{Ipk} = \frac{DutyI \times VFEF_IN}{2ILED} \quad (2)$

Ipk: peak inductor current Vf: LED forward voltage drop Vac: effective value(R.M.S value) VREF: Built-in reference voltage (0.605V) VREF_IN: REF_IN voltage (6 pin) Rs: External sense resistor Vzd: Zener diode voltage (REF_IN pin)

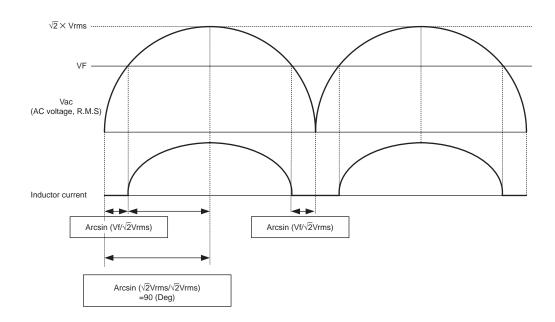
Since formula for LED current is different between on period and off period as shown above,

 $Ipk \times \frac{Vac - Vf}{L} \times T_{c} = \frac{Vf}{L} \times T_{d} \quad (3)$ Since $T_{c} + T_{d} = DutyI \times T$, $T_{c} = DutyI \times T - T_{d} \quad (4)$ Based on the result of (3) and (4), $T_{d} = DutyI \times T \times \frac{Vac - Vf}{Vac} \quad (5)$

To obtain L from the equation (1), (3), (5),

$$L \times \frac{Vf \times DutyI}{2 \times ILED} \times DutyI \times T = \frac{Vac - Vf}{Vac} = \frac{Vf}{2 \times ILED} \times \frac{1}{fosc} \times \frac{Vac - Vf}{Vac} \times (DutyI)^2 \quad (6)$$

Since LED and inductor are connected in serial in non-isolation mode, LED current flows only when AC voltage exceed VF.



Given that the ratio of inductor current to AC input is DutyAC.

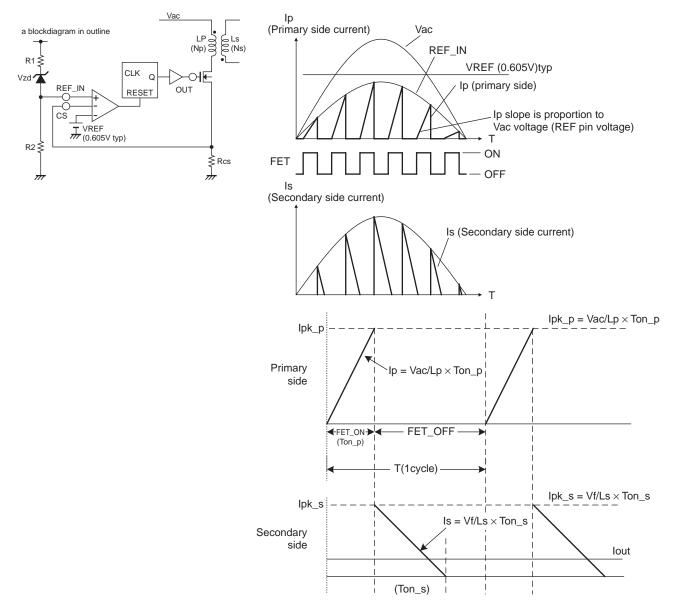
$$DutyAC = \frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)}{90}$$

Since the period when the inductor current flows are limited by DutyAC, the formula (6) is represented as follows:

$$L = \frac{Vf}{2 \times ILED} \times \frac{1}{fosc} \times \frac{Vac - Vf}{Vac} \times (DutyI)^2 \left(\times \frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)^2}{90} \right)^2$$
(7)

(for Isolation circuit)

Using the circuit diagram below, the wave form of the current that flows to Np and Ns is as follows. Current waveform flows to primary side and secondary.



[Inductance Lp of primary side and sense resistor Rs]

If a peak current flow to transformer is represented as Ipk_p, the power (Pin) charged to the transformer on primary side can be represented as:

$$Pin = \frac{1}{2} \times Lp \times (Ipk_p)^2 \times fosc \quad (11)$$

$$Ipk_p = \frac{Vac}{Lp} \times Ton_p \quad (12)$$

$$Lp = \frac{Vac^2 \times Ton_p^2 \times fosc}{2 \times Pin} = \frac{Vac^2 \times Don_p^2}{2 \times Pin \times fosc} \quad (13)$$

$$(Don_p = \frac{Ton_p}{T} = Ton_p \times fosc),$$

To substitute the following to the formula below,

$$\therefore \eta = \frac{Pout}{Pin} \quad (14)$$
$$\therefore Lp = \frac{Vac^2 \times Ton_p^2 \times fosc \times \eta}{2 \times Pout} = \frac{Vac^2 \times Don^2 \times \eta}{2 \times Pout \times fosc} \quad (15)$$

Sense resistor is obtained as follows.

$$Rs = \frac{VREF_IN}{Ipk_p} = \frac{VREF_IN \times Lp}{Vac \times Ton_p} = \frac{VREF_IN \times Lp}{Vac \times Don_p \times T}$$
(16)
[Inductance Ls of secondary side]

Since output current lout is the average value of current flows to transformer of secondary side

$$Iout = Ipk_s \times \frac{Ton_s}{T} \times \frac{1}{2} = \frac{Ipk_s \times Don_s}{2} (Don_s = \frac{Ton_s}{T} = Ton_s \times fosc)$$
(17)
$$Ipk_s = \frac{Vout}{Ls} \times Ton_s = \frac{Vout}{Ls} = \frac{Don_s}{fosc}$$
(18)
$$Ls = \frac{Vout \times T \times Don_s^{2}}{2 \times Iout} = \frac{Vout \times Don_s^{2}}{2 \times Iout \times fosc} = \frac{Vout^{2} \times Don_s^{2}}{2 \times Pout \times fosc}$$
(19)

Calculation of the ratio of transformer coil on primary side and secondary side Since ratio and inductance of transformer coil is

$$\frac{Ns}{Np} = \frac{\sqrt{Ls}}{\sqrt{Lp}} \quad (20)$$

substituted equations (15), (19) for (20)

$$\therefore \frac{Np}{Ns} = \frac{Vac}{Vout} \times \sqrt{\eta} \times \frac{Don_p}{Don_s} \quad (21)$$

Calculation of transformer coil on primary side and secondary side

$$N = \frac{Vac \times 10^8}{2 \times \Delta B \times Ae \times fosc} \quad (22)$$

 $\label{eq:alphaB} \begin{array}{l} \Delta B: \mbox{variation range of core flux density [Gauss]} \\ Ae: \mbox{core section area } [\mbox{cm}^2] \end{array}$

To use Al (L value at 100T),

$$N = \sqrt{\frac{L}{Al}} \times 10^2 \quad (23)$$

L: inductance [µH] Al: L value at 100T [uH/N²] lg (Air gap) is obtained as follows:

$$\lg = \frac{\mu_{\rm r} \, \mu_0 \, N^2 \, A_e \, 10^2}{L} \quad (24)$$

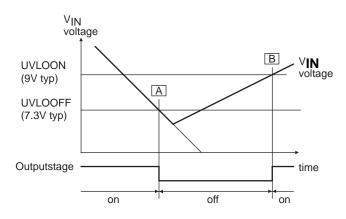
μr: relative magnetic permeability, μr = 1 μ0: vacuum magnetic permeability μ0 = $4\pi * 10^{-7}$ N: turn count [T] Ae: core section area [m²] L: inductance [H]

Description of operation Protection function

	tilte	outline	monitor point	note			
1	UVLO	Under voltage lock out	V _{IN} voltage				
2	OCP	Over current protection	CS voltage	available FET current			
3	OVP	Over voltage protection	V _{IN} voltage				
4	OTP	Over Temperature Protection	PN Junction temperature				
	(TSD)	(Thermal Shut Down)					

1. UVLO (Under voltage lock out)

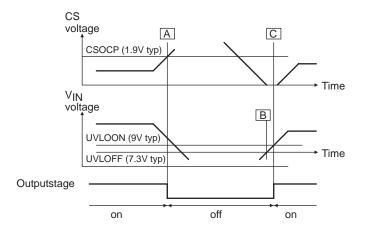
If V_{IN} voltage is 7.3V or lower, then UVLO operates and the IC stops. When UVLO operates, the power supply current of the IC is about 80µA or lower. If V_{IN} voltage is 9V or higher, then the IC starts switching operation.



2. OCP (Over current protection)

The CS pin senses the current through the MOS FET switch and the primary side of the transformer. This provides an additional level of protection in the event of a fault. If the voltage of the CS pin exceeds VCSOCP (1.9V typ) (\overline{A}), the internal comparator will detect the event and turn off the MOSFET. The peak switch current is calculated Io (peak) [A] = VSOCP [V]/Rsense [Ω]

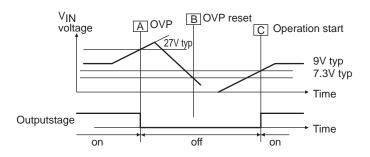
The V_{IN} pin is pulled down to fixed level, keeping the controller latched off. The latch reset occurs when the user disconnects LED from VAC and lets the V_{IN} falls below the V_{IN} reset voltage, UVLOOFF (7.3V typ)(\boxed{B}). Then V_{IN} rise UVLOON (9V typ) (\boxed{C}), restart the switching.



3. OVP (Over voltage protection)

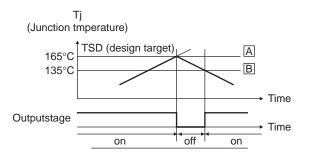
If the voltage of V_{IN} pin is higher than the internal reference voltage $V_{IN}OVP$ (27V typ), switching operation is stopped.

The stopping operation is kept until the voltage of V_{IN} is lower than 7.3V. If the voltage of V_{IN} pin is higher than 9V, the switching operation is restated.



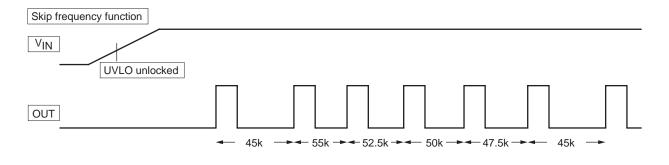
4. OTP (Over temperature protection)

The over temperature protection function works when the junction temperature of IC is $165^{\circ}C$ (typ) (A), and the IC switching stops. The IC starts switching operation again when the junction temperature is $135^{\circ}C$ typ (B) or lower.



Skip frequency function

LV5029MD contains the skip frequency function for reduction of the peak value of conduction noise. This function changes the frequency as follows.



Switching frequency is changed as follows. $\dots \times 0.9 \rightarrow \times 1.1 \rightarrow \times 1.05 \rightarrow \times 1 \rightarrow \times 0.95 \rightarrow \times 0.9 \rightarrow \times 1.1 \dots$ It's repeated by this loop.

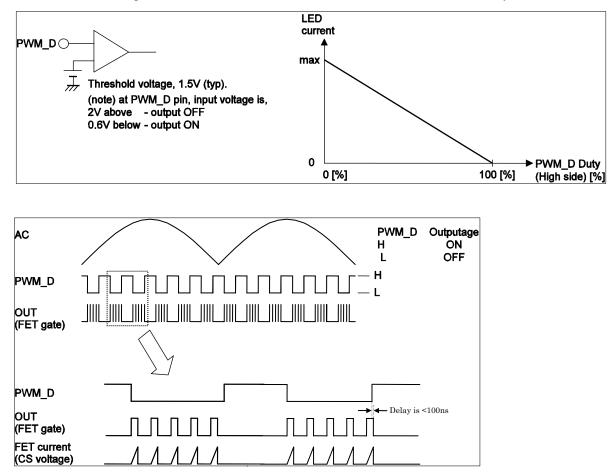
PWM dimming function

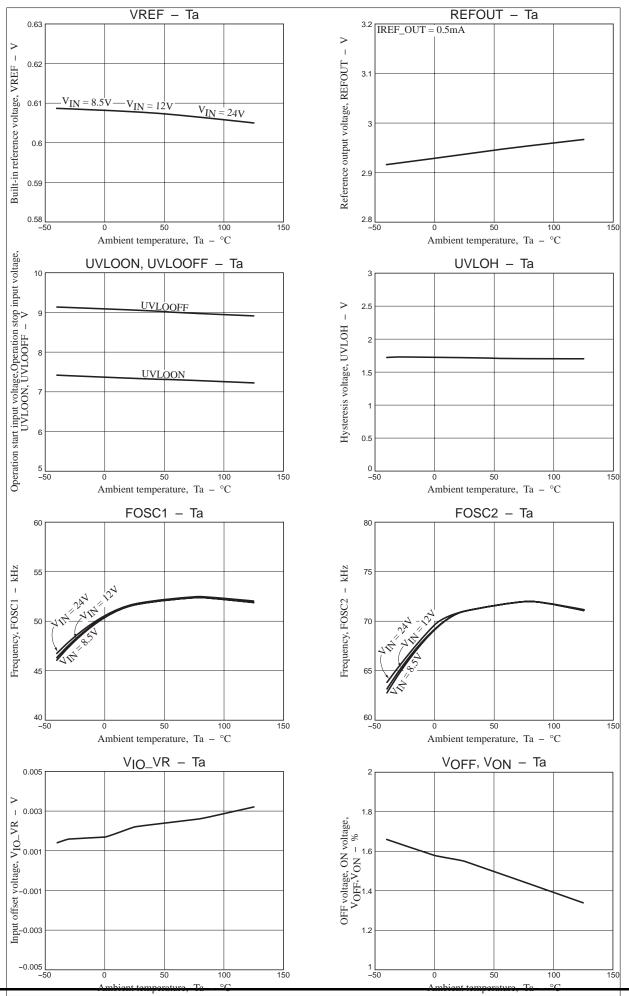
LED current can be adjusted according to Duty of PWM pulse input to PWM dimmer pin. PWM pulse is High (2V to 5V) then switching operation stops, and LED current stops flowing. PWM pulse is Low (under 0.6V), then switching operation stop is released, and it returns to normal operation. The OUTPUT FET is turned OFF within 100ns if PWM input turns into High when the OUTPUT FET is turned on.

<u>The recommended frequency of PWM dimming input is 100Hz (twice the AC voltage frequency) to 5 kHz.</u> When frequency of the PWM is less than twice the AC frequency, a flicker becomes easy to be observed. On the other hand, if PWM frequency rise to around 50 kHz that is driving frequency of the switching of the OUTPUT FET, the flicker is easy to occur.

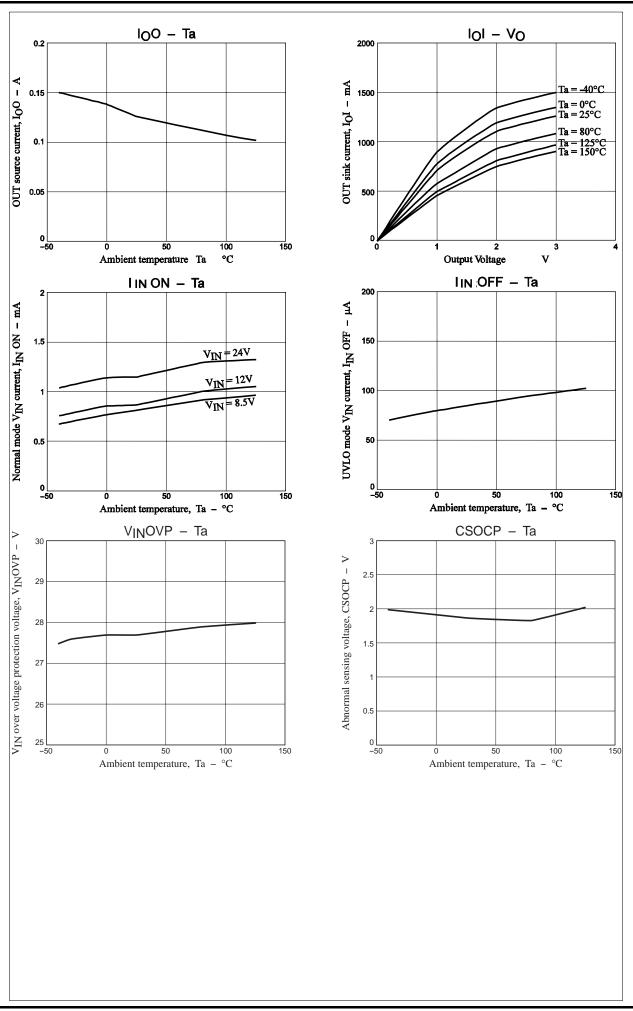
An outline of PWM_D pin

LED current vs PWM_D duty (outline)





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